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大米发酵渣、液对脱硫石膏性能的影响

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摘要:将大米发酵渣(RR)和发酵液(RL)用于脱硫石膏(DG)砌块。结果表明:RR、RL可作为DG外加剂,具有增加DG标准稠度用水量、缓凝时间、吸水率和软化系数的作用;添加0.9%的RR、RL后,DG的软化系数分别增加了41.9%和35.4%,吸水率分别提升了57.9%和57.0%;RR、RL对DG的力学性能具有负面影响,但其力学衰减程度与常见盐类外加剂相当;大米发酵物具有影响DG中二水硫酸钙(002)面生长的作用,但两者未形成共价键连接,且二水硫酸钙的晶体形貌未发生明显变化。

关键词:脱硫石膏;大米发酵物;软化系数;缓凝时间

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Impact of Rice Fermentation Residue and Liquid on Performance of Desulfurization Gypsum

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Abstract: Rice fermentation residue and liquid were used in desulfurization gypsum blocks as admixtures. The results indicate that these admixtures effectively increase the standard consistency water requirement, retard setting time and enhance water resistance of desulfurization gypsum. Specifically, after adding 0.9% rice fermentation residue and liquid, the softening coefficients increase by 41.9% and 35.4%, respectively, while the water absorption rates decrease by 57.9% and 57.0% compared to the blank control group. Although rice fermentation residue and liquid negatively affect the mechanical properties of desulfurization gypsum, the degree of mechanical property reduction is comparable to that of common salt based admixtures. Additionally, rice fermentation products influence the growth of the (002) plane of calcium sulfate dihydrate without forming covalent bonds with the crystals, and the morphology of dihydrate gypsum crystals remains largely unchanged.

Key words: desulfurization gypsum; rice fermentation product; waterproof performance; softening coefficient; retardation time

中国发电结构仍以燃煤发电为主,在这个过程中会产生大量的固体废弃物脱硫石膏(DG)^[1-4]。受限于国家环保政策和工程需求,行业亟需通过技术手段提升DG的性能。酒糟作为酿酒工业的主要副产物,直接排放会导致生态系统失衡,加剧环境污染^[5-9]。将酒糟应用于DG性能优化,可有效降低这

种废弃物的环境负荷。

为使石膏性能满足工程需要,常在配方设计时添加外加剂,以调整石膏浆体的稠度、缓凝时间、吸水率、软化系数和力学性能等。已有研究表明,用于石膏中的蛋白质缓凝剂具有出色的缓凝效果^[10-11]。Ding等^[12]发现水解小麦蛋白能抑制石膏的水化并具

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有缓凝作用。Xu等^[13]研究了不同氨基酸对石膏水化的抑制作用。Fang等^[14]证明聚天冬氨酸(PASP)通过吸附在石膏颗粒表面显著降低了石膏的初始溶解度。大米发酵物经提取乙醇后,发酵废物主要成分的结构与多糖类、蛋白质类石膏外加剂类似。理论上,大米发酵渣(RR)和米发酵液(RL)对于石膏应具有类似效应,但现有研究未揭示其效果。

本研究首次将RR、RL用于DG制品,评估其对DG浆体宏观性能及微观结构的影响。首先,研究RR、RL对DG标准稠度用水量、凝结时间、力学性能、吸水率和软化系数等宏观性能的影响。其次,采用X射线衍射仪(XRD)、傅里叶转换红外光谱仪(FTIR)和扫描电镜(SEM)研究改性前后石膏硬体的物相组成、化学键和形貌。最后,建立DG制品综合性能的相关性数学模型。

1 试验

1.1 原材料

DG粉体呈针棒状,中位粒径 $26.37\ \mu\text{m}$ 。RR、RL为实验室自制,其制作方法为:首先,将2000 g大米浸泡24 h后放入10 g酵母和200 mL水,搅拌均匀并在 $25\ ^\circ\text{C}$ 陈放24 h;随后,加入3000 mL温度为 $35\ ^\circ\text{C}$ 的去离子水拌匀,再将拌匀好的物料倒入发酵筒,在 $25\ ^\circ\text{C}$ 环境下密封发酵一周后,用滤布将渣和液分离;最后,将发酵后的渣放入烘箱(温度不超过 $40\ ^\circ\text{C}$)中干燥后破碎并研磨成粉状。分离后的液体经提纯乙醇后,形成废液^[15]。RR呈团状,表面粗糙,中位粒径 $190.20\ \mu\text{m}$ 。图1为DG的XRD图谱。图2为RR的热重-微商热重(TG-DTG)曲线。由图2可见,RR在 $200\ ^\circ\text{C}$ 时开始分解并且在 $600\ ^\circ\text{C}$ 时几乎完全分解。

1.2 样品制备与检测方法

根据GB/T17669.4—1999《建筑石膏净浆物理性能的测定》,制备RR、RL改性石膏样品,其中RR、RL掺量(w)为DG粉用量的0%(对照组样品control)、0.1%、0.3%、0.5%、0.7%、0.9%。根据上述标准和文献^[16],测定改性石膏的标准稠度用水量、缓凝时间、力学性能、吸水率和软化系数。采用日本理学D/max 2550 VB 3+型XRD进行相分析,Cu K α ($k=0.154\ 1\ \text{nm}$)靶,步进扫描,步长 0.02° ,范围 $3^\circ\sim 70^\circ$ 。采用FTIR-NEXUS-670型FTIR,光谱范围为 $4\ 000\sim 400\ \text{cm}^{-1}$,分辨率为 $4\ \text{cm}^{-1}$ 。采用FEI QUANTA 200 FEGSEM型SEM进行微观形貌分析,碳基导电胶,观察部位为样品中心断裂面,未进行喷金处理。

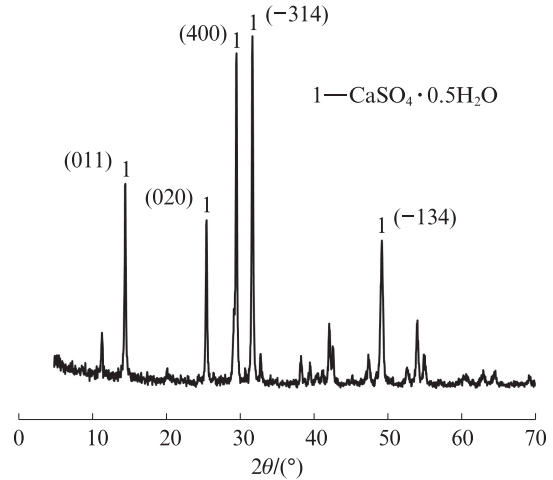


图1 DG的XRD图谱
Fig. 1 XRD pattern of DG

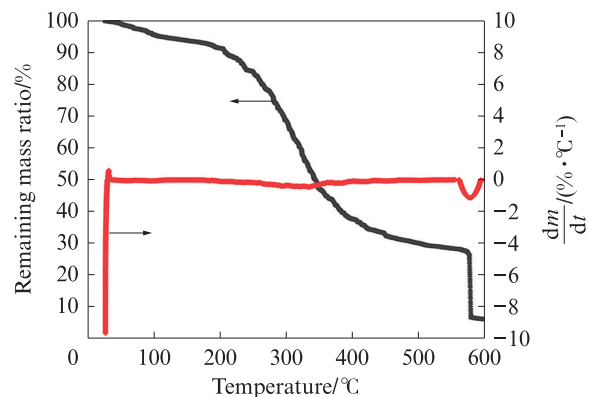


图2 RR的TG-DTG曲线
Fig. 2 TG-DTG curves of RR

2 结果与讨论

2.1 标准稠度及固定用水量

图3为RR和RL对DG标准稠度及用水量的影响。由图3可见:RR和RL具有增加DG标准稠度用水量的效果,可以改善DG在高水灰比条件下的泌水现象;与不掺RR和RL的空白样相比,掺加

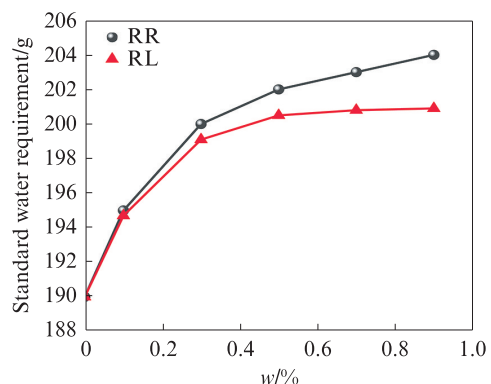
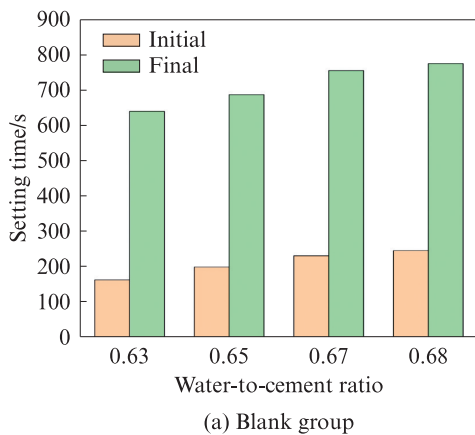


图3 RR和RL对DG标准稠度及用水量的影响
Fig. 3 Effect of RR and RL on standard consistency and water consumption of DG

0.9%RR DG样品的标准稠度提升了7.3%,掺加0.9%RL DG样品的标准稠度提升了5.7%,RR的增稠效果优于RL。一般而言,提高DG的标准稠度用水量可以减少DG粉的用量。因而,在DG砌块的生产过程中,当满足应用需求时,应减少DG粉用量以达到经济效益。Zhu等^[17]采用预糊化淀粉实现了高水灰比条件下制备石膏砌块的目标。但是,预糊化淀粉改性石膏具有低软化系数的特征。尽管本试验中RR、RL对DG标准稠度的提升能力远不如预糊化淀粉,但其软化系数高于预糊化淀粉改性石膏体系。

2.2 凝结时间

图4为RR和RL对DG凝结时间的影响。由图4可见:由RR和RL具有缓凝效果;在相同水灰比时,纯DG体系的凝结时间小于RR、RL改性DG体系;与样品control相比,掺加0.9%RR DG样品



的初凝时间提升了200%,终凝时间提升了108%,掺加0.9%RL DG样品的初凝时间提升了150%,终凝时间提升了46%。

2.3 力学性能

图5为RR和RL对DG强度的影响。由图5可见,与样品control相比,掺加0.9%RR DG样品的分别下降了29.2%和22.3%,掺加0.9%RL DG样品的下降了27.7%和21.6%。RR、RL对DG力学性能具有负面影响,但其力学衰减程度与常见盐类外加剂的相当^[18]。理论上,随着水含量的增加,石膏硬化体由于水挥发而引入更多孔隙,从而引起强度下降。以标准稠度用水量作为参考依据时,强度降低应与用水量增加有关。在工程应用中,石膏砌块的抗压强度应不低于3.5 MPa。本实验制备样品的抗压强度均高于此值,表明以RR、RL改性DG为基础的配方,可降低DG粉用量,提高经济效益。

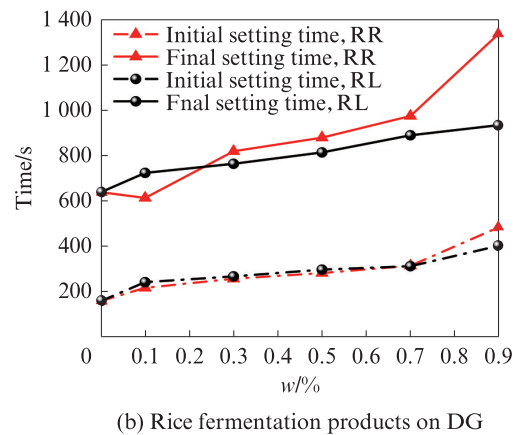


图4 RR和RL对DG凝结时间的影响

Fig. 4 Effect of RR and RL on setting time of DG

2.4 吸水率和软化系数

图6为标准稠度下不同大米发酵物含量对软化系数和吸水率的影响。由图6可见:

(1)在相同水灰比时,纯石膏体系的软化系数和吸水率均小于RR、RL改性石膏。

(2)当大米发酵物掺量为0.9%时,RR改性石膏样品的软化系数为0.44,RL改性石膏样品的软化系数为0.42,相较于样品control分别提升了41.9%和35.5%。

(3)当大米发酵物掺量为0.9%时,RR改性石膏样品的吸水率为0.169,RL改性石膏样品的吸水率为0.168,相较于样品control分别提升了57.9%和57%。一般而言,石膏的吸水率降低软化系数增加,但本研究的发现与经验规律不同,随着RR、RL掺量的增加,DG的吸水率和软化系数均呈现上升趋势。

Zhu^[17]等利用分子动力学模拟发现淀粉类物质具有增强石膏接触点的作用。由于RR、RL中含有淀粉降解物,软化系数提升可能源于石膏接触点增强。

2.5 宏观性能相关性分析

图7为掺入大米发酵物后DG标准稠度用水量与软化系数和吸水率的关系图。

由图7(a)、(b)可见,RR掺入后,软化系数与用水量呈现 $y=ax+b$ 的线性趋势,吸水率和用水量相关性,符合方程 $y=a+b\frac{e^{kx-1}}{k}$ 。

由图7(c)、(d)可见,RL掺入后,软化系数和用水量相关性、吸水率和用水量相关性,均满足方程 $y=a+b\frac{e^{kx-1}}{k}$ 。

Wu等^[19]研究了硅烷改性苯乙烯-丙烯酸乳液对

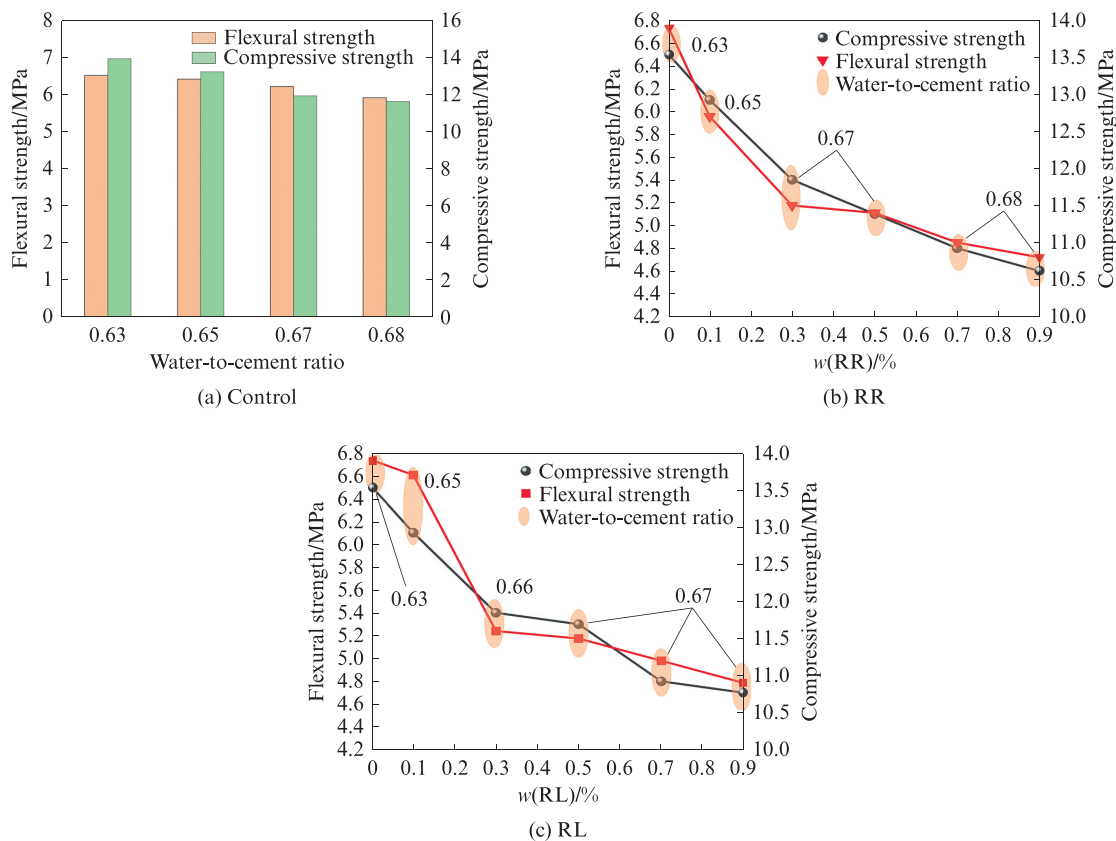


图5 RR和RL对DG强度的影响
Fig. 5 Effect of RR and RL on strength of DG

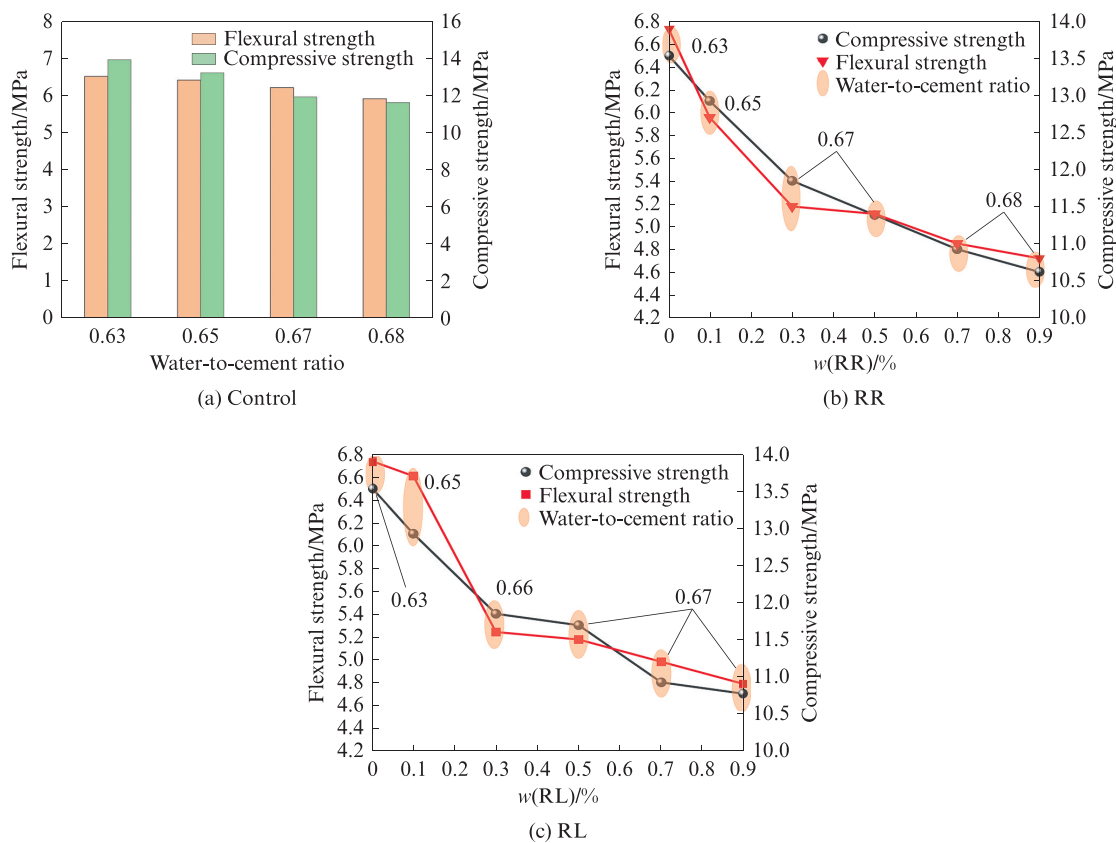


图6 标准稠度下不同大米发酵物含量对DG软化系数和吸水率的影响
Fig. 6 Impact of rice fermentation product content on softening coefficient and water absorption rate of DG under standard consistency

烟气脱硫(FGD)石膏吸水率和软化系数的影响,结果表明吸水率与软化系数呈现负相关趋势。在本研究中,吸水率与软化系数呈现正相关。

图8为对于大米发酵物改性石膏的综合性能评估图。在实际工程中,石膏强度只需达到3.0 MPa,本研究所述配方强度达标。由图8可见,相较于样品

control,0.9%RR改性DG的软化系数和吸水率分别增长了41.9%和57.9%,0.9%RL改性DG的软化系数和吸水率分别增长了35.4%和57.0%。总之,RR改性DG的综合性能优于RL改性DG。

2.6 物相分析

图9为样品的XRD图谱^[20-23]。由图9可见:所有

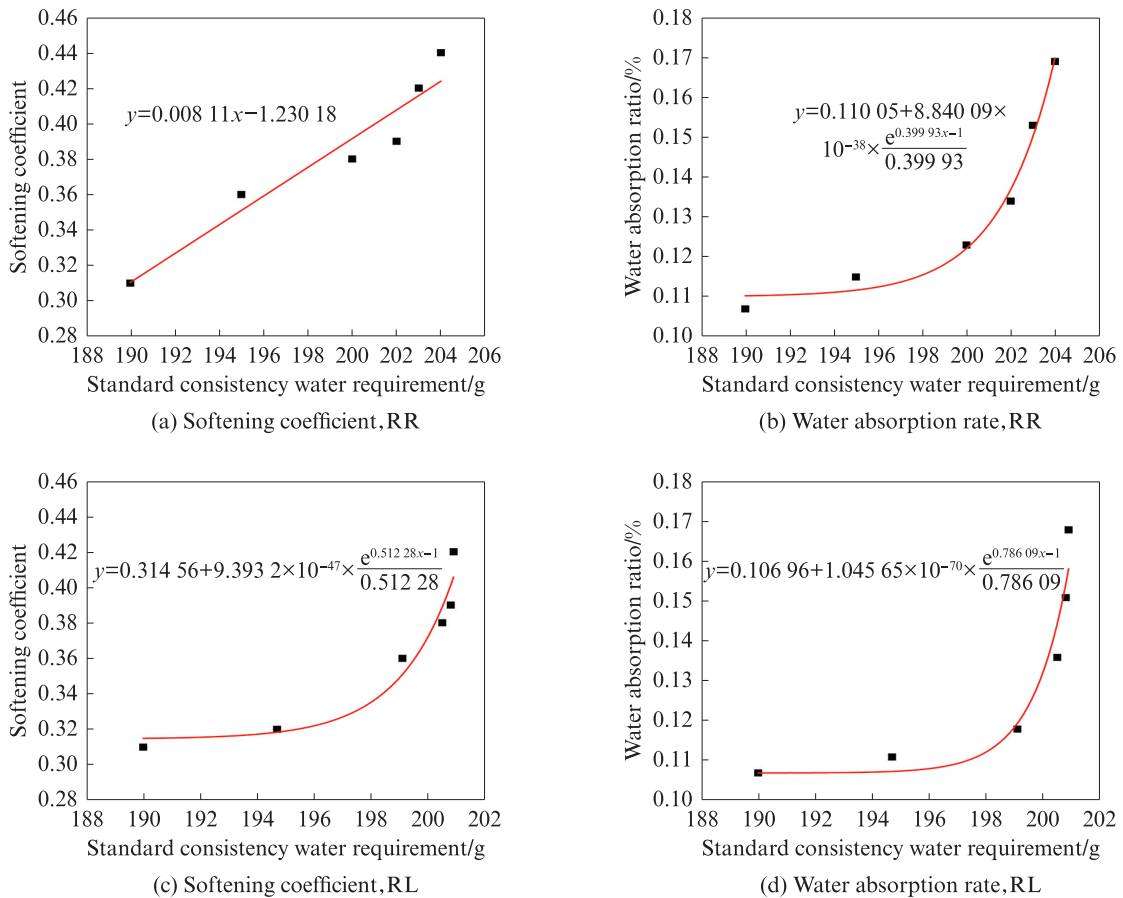


图7 掺入大米发酵物后DG标准稠度用水量与软化系数和吸水率的关系图

Fig.7 Graph showing the fitting function of water usage for fermented rice addition versus softening coefficient and water absorption rate of DG

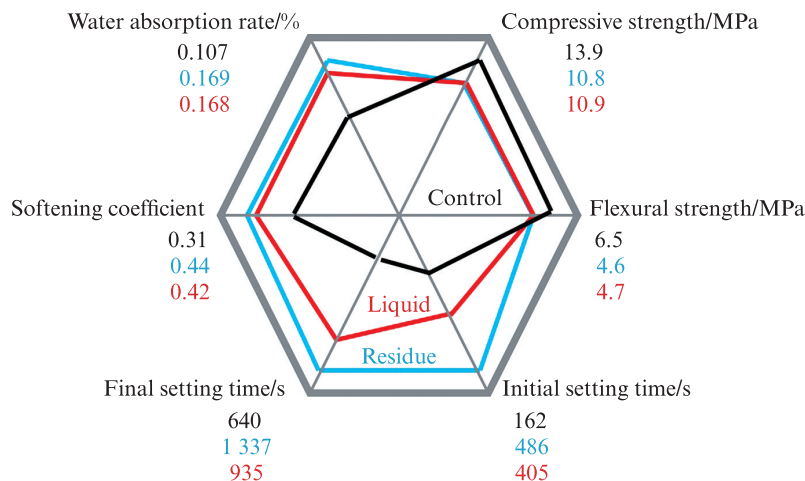


图8 大米发酵物改性石膏的综合性能

Fig.8 Comprehensive performance of DG modified by rice fermentation products

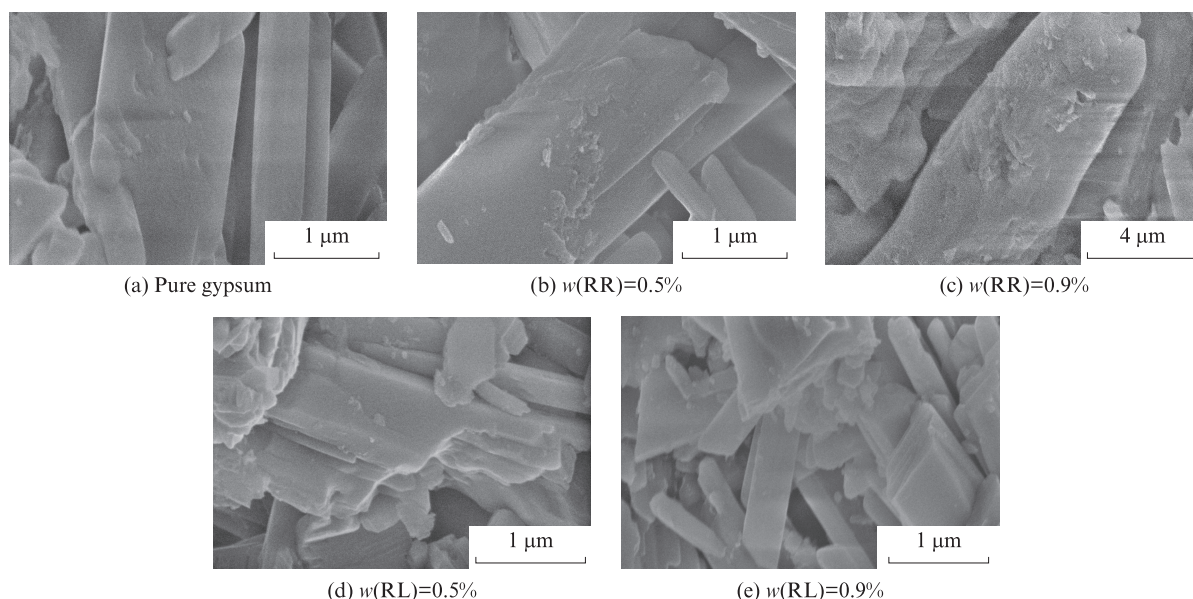


图11 样品的SEM照片

Fig. 11 SEM images of samples

3 结论

(1)大米发酵渣(RR)和发酵液(RL)可作为脱硫石膏(DG)外加剂,具有提升DG标准稠度用水量、吸水率和软化系数的作用。添加0.9%的RR、RL后DG软化系数分别增加了41.9%和35.4%,而吸水率相较于对照组样品分别提升了57.9%和57.0%。RR掺入后,DG的软化系数与用标准稠度水量为正相关。RR、RL对DG水化具有缓凝作用,且其对DG力学性能具有负面影响,力学衰减程度与常见盐类外加剂的相当。

(2)RR、RL具有影响DG中二水硫酸钙(002)面生长的作用,未与二水硫酸钙晶体形成共价键连接,且晶体形貌未发生明显变化。

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